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## STUDY OF AERODYNAMIC INTERFERENCE EFFECTS ON AERODYNAMIC COEFFICIENTS OF TWIN-DECK BRIDGES

CHEN Zheng-qing , \*LIU Xiao-bing , LIU Zhi-wen

(Wind Engineering Research Center, Hunan University, Changsha, Hunan 410082, China)

**Abstract:** There exist aerodynamic interference effects between the windward deck and the leeward deck of twin-deck bridges under wind load. Aerodynamic interference effects on aerodynamic coefficients of a twin-deck bridge were investigated with a series of section-model wind tunnel tests using both force-measurement method and pressure-measurement method. The results show that the aerodynamic interference effects on drag coefficients of twin-deck bridges could not be neglected. Compared with single deck alone, the drag coefficients of leeward deck are much smaller and those of windward deck decrease slightly. The aerodynamic interference effects on the lift and torque coefficients of twin-deck bridge could be ignored.

**Key words:** twin decks; aerodynamic coefficients; aerodynamic interference; force-measurement method; pressure-measurement method

[1-4]

Memorial Bridge Pearl Harbor Fairway Bridge( Sarkar P P<sup>[5]</sup> Tsurumi  
Fred Hartman Bridge )  
( )

2006-12-06

2007-05-22

(50608030)

(50478051)

(E-mail: zqchen@hnu.cn)

(1947-)

\* (1982-)

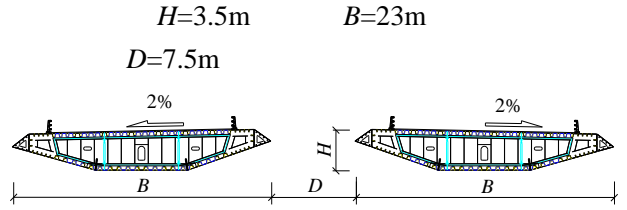
(1975-)

(E-mail: x\_b\_liu@126.com)

(E-mail: liuzhiwen757@126.com).

Akihiro Honda<sup>[6]</sup>  
Airport Access Bridge( )

Kansai International



1  
Fig.1 Cross section of girder

[7-8]

( )

2%

DS(

) DX(

) S( )

1

$D/H=1.0$   $D/H=2.143$ ( )

$D/H=4.0$

( $D/H=2.143$ )

2

3

1

3

HD-2

17.0m

60.0m+120.0m+

2.5m

3.0m

10m/s

120.0m+60.0m=360.0m

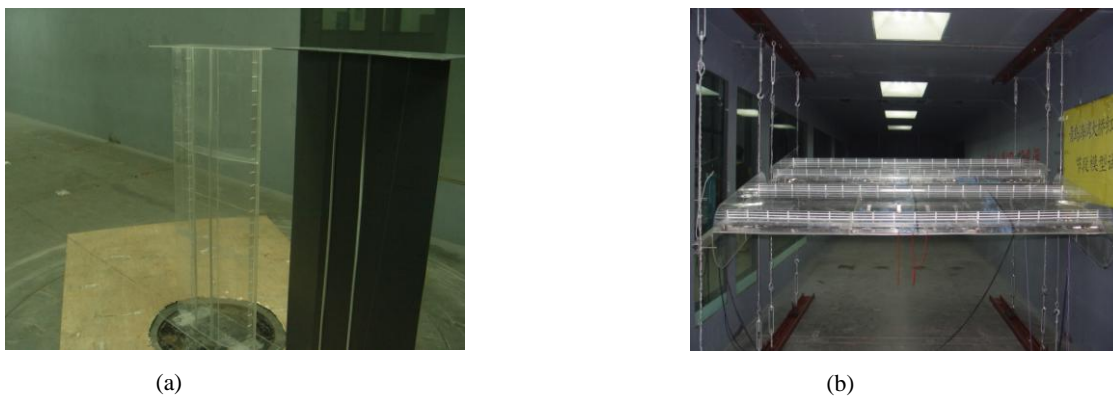
1

0.4%

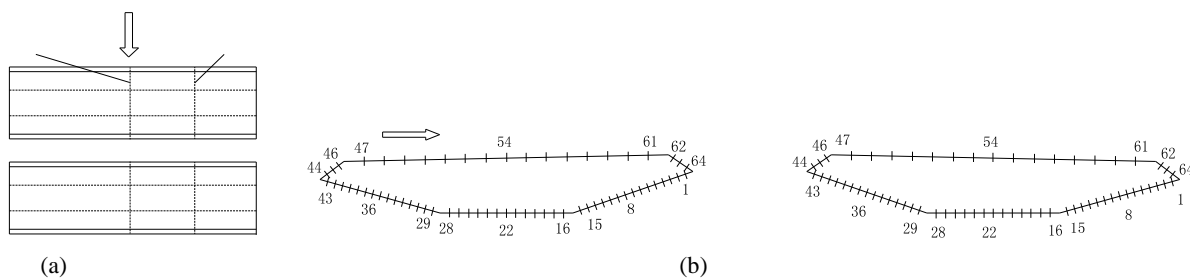
1

Table1 Cases of wind tunnel tests

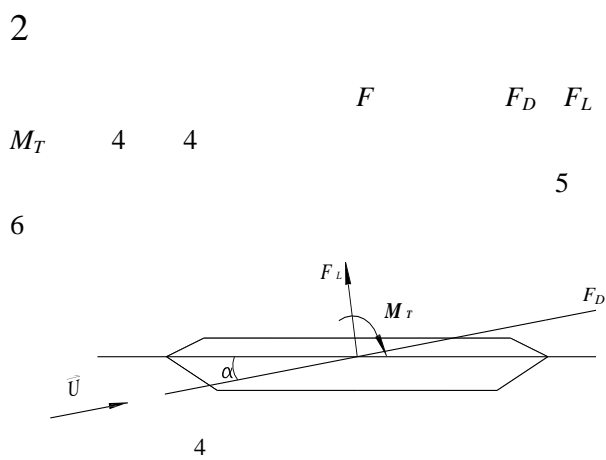
1			DS	
2	1/50		DX	
3			$S(D/H=1.0)$	$-10^{\circ} \sim -10^{\circ}$
4			$S(D/H=2.413)$	
5			$S(D/H=4.0)$	
6	1/25		$S(D/H=2.413)$	



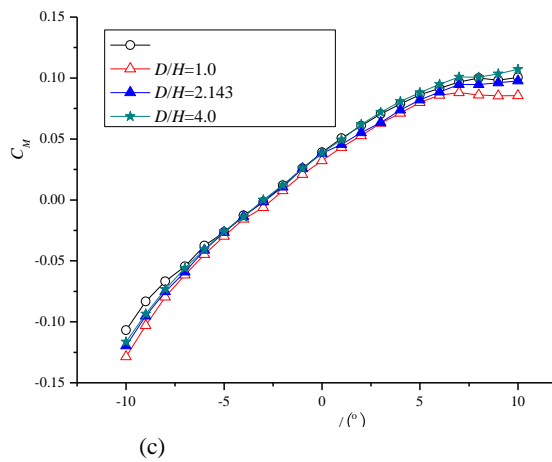
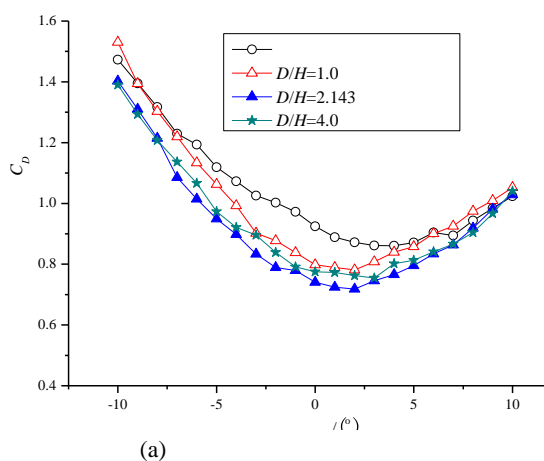
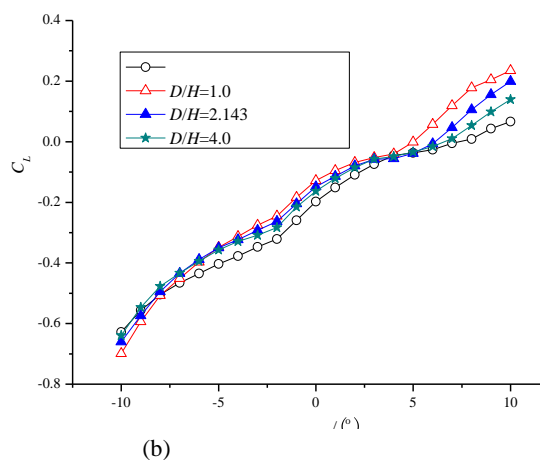
2  
Fig.2 Photos of wind tunnel tests

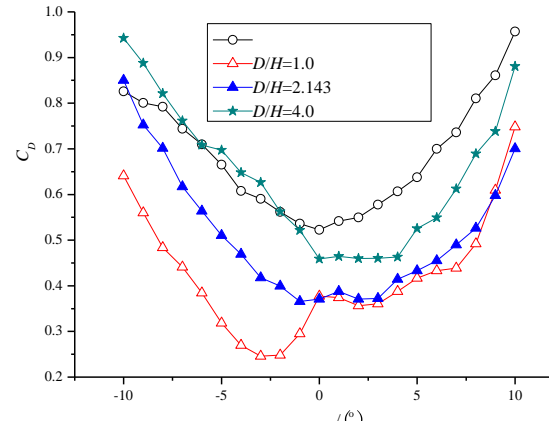


3  
Fig.3 Pressure taps location and numbers

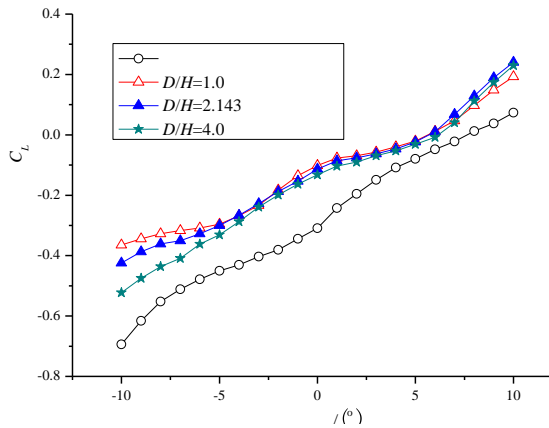


4  
Fig.4 Aerodynamic forces in wind coordinate system

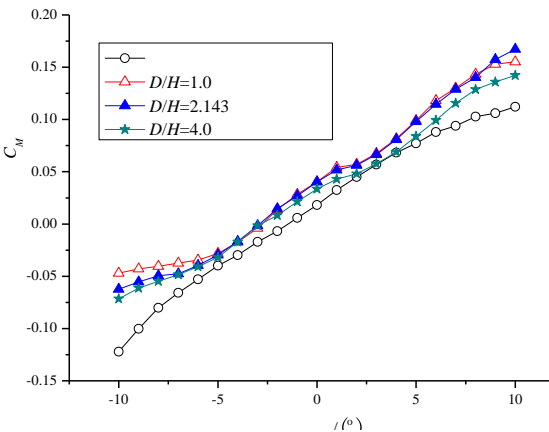




(d)



(e)



(f)

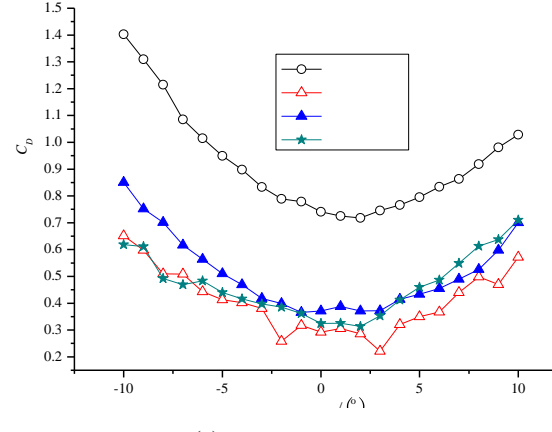
5  
Fig.5 Force-measurement results

$$C_D = 2F_D / \rho U^2 DL \quad (1)$$

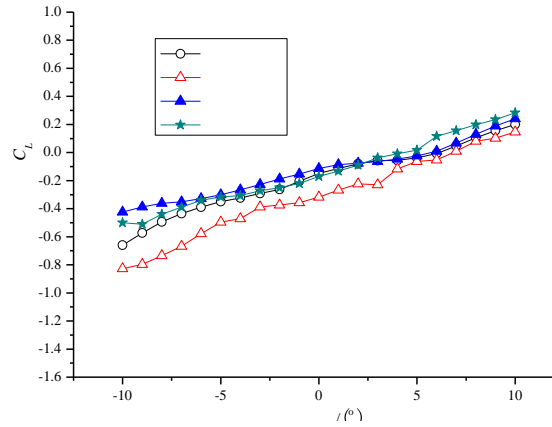
$$C_L = 2F_L / \rho U^2 BL \quad (2)$$

$$C_M = 2M_T / \rho U^2 B^2 L \quad (3)$$

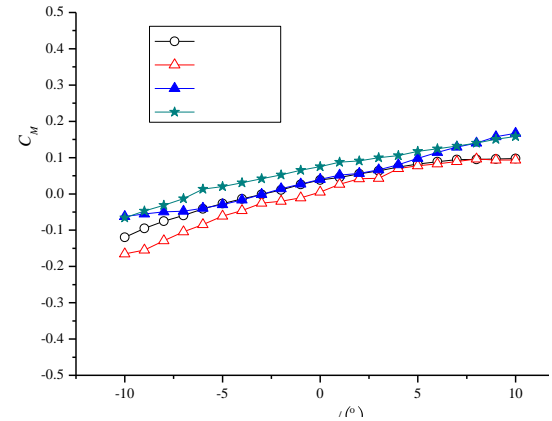
$D$     $B$     $L$   
 $U$                        $\rho$                        $1.225\text{kg/m}^3$



(a)



(b)



(c)

6  
Fig.6 Comparisons of force-measurement results and pressure-measurement results

5

1)

“ ”

2)

“ ”

3

3)

-5° 5°

6

7

(D/H=

2.143) 0° -10°

$$C_i = (P_i - P_\infty) / 0.5 \rho U^2 \quad (4)$$

$C_i$   $P_i$   $P_\infty$   $i$

Hangan H  
delli F<sup>[9]</sup>

Regio Calabria

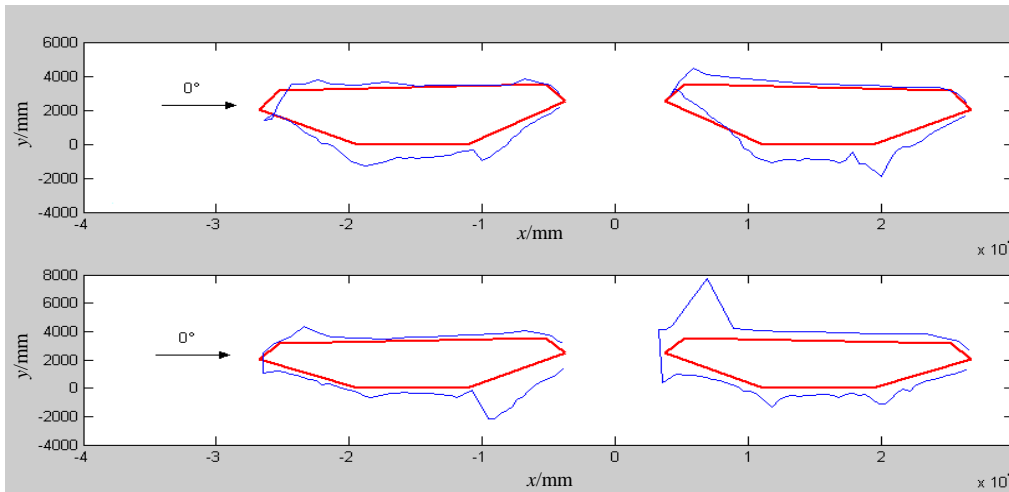
Ricciar-  
[10]

$i$

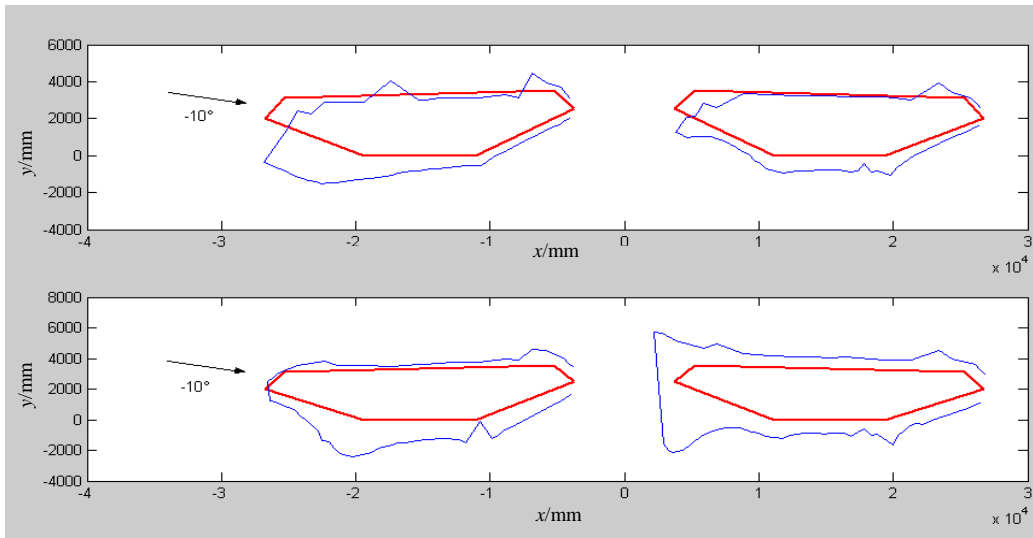
7

2/3

7  
1500 15000



(a) 0°



(b)  $-10^\circ$

7

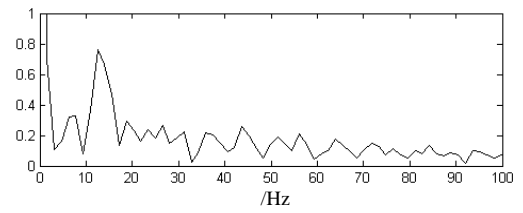
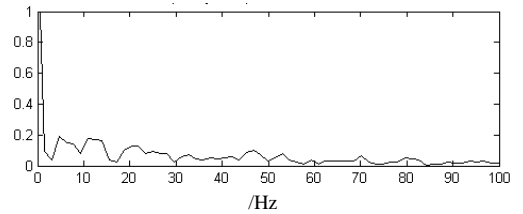
Fig.7 Mean and RMS pressure coefficient of twin decks at various wind attack angles

7

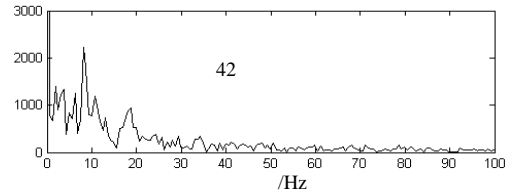
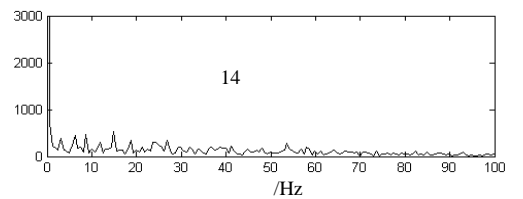
$0^\circ$   
“ ”

$0^\circ -10^\circ$

“ ”  $0^\circ$   
 $-10^\circ$



(a)  $0^\circ$



(b)  $-10^\circ$

8

Fig.8 Magnitude spectrum of aerodynamic coefficients and single tap pressure coefficients of twin decks

8

4

(1)

(2)

“ ”

(3)

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